

GENERAL CERTIFICATE OF EDUCATION BOARD

Technical and Vocational Education Examination

JUNE 2021

ADVANCED LEVEL

| | |
|-----------------------|------------------------------------|
| Specialty Name / Code | Electrical Power Systems (EPS) |
| Subject Title | Design of Electrical Installations |
| Subject Code N° | 7245 |
| Paper N° | 2 |

Three hours

The paper has Two Sections (A and B) and constitutes 35% of the whole subject.

Section A has ONE COMPULSORY QUESTION, carrying 40 marks.

Section B has FOUR QUESTIONS, each carrying 30 marks. ANSWER ANY TWO QUESTIONS.

All sketches must be neat and clear.

You are allowed the use of Electronic calculators and mathematical sets.

No programmable calculators are allowed

You are also reminded of the necessity for good English and orderly presentation in your answers.

You are advised to read carefully through the question paper, before you begin your answers.

We want to realize a preliminary design of electrical installation of a newly created GTHS which will offer three trades for the beginning, consisting of three workshops, an administrative block and twelve (12) class rooms.

I. General Presentation.

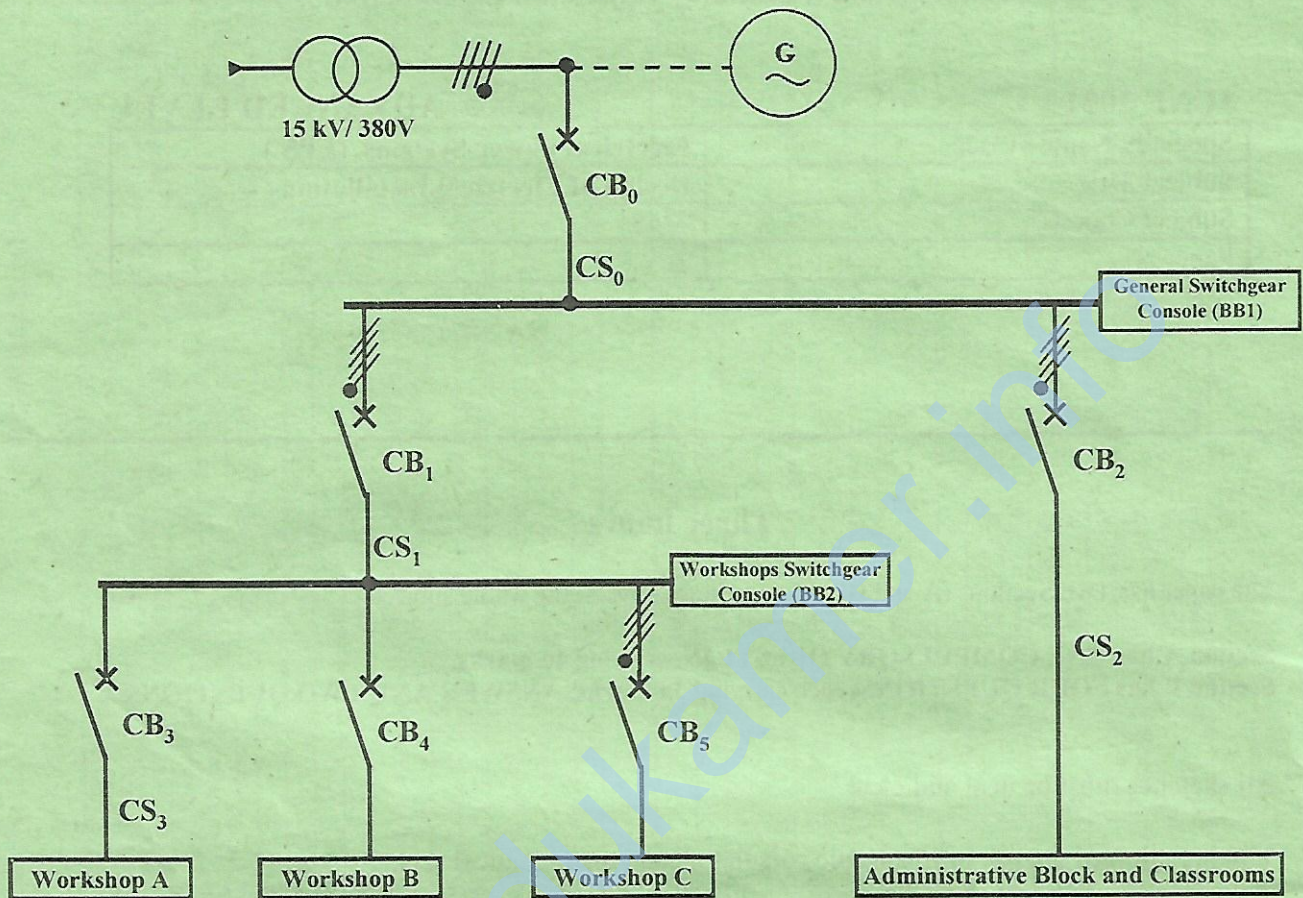


Figure 1: General Line Diagram of the Installation

II. Presentation of the Different Blocks.

Workshop A : Motor mechanics.

- Six (06) 1-ph motors: $P = 1.5kW$; $\cos \varphi = 0.70$; $\eta = 0.7$ each. $K_S = 0.75$; $K_U = 0.8$
- Eight (08) 1-ph socket-outlets of $2P + T$; 16A, 220V each.
- 30 fluorescent tubes of 40W; $\cos \varphi = 0.86$.
- A 15kW compressor of $\cos \varphi = 0.85$; $\eta = 0.7$; $K_U = 0.8$
- A 15kW lift of $\cos \varphi = 0.75$; $\eta = 0.75$; $K_U = 0.8$

Workshop B: Mechanical manufacturing.

- Twenty (20) compensated fluorescent tubes of 58W; $\cos \varphi = 0.86$ each.
- Ten (10) 1-ph socket-outlets of $2P + T$; 16A, 220V each.
- Four (04) 1-ph motors of: $P = 2.2kW$; $\cos \varphi = 0.80$; $\eta = 0.75$ $K_S = 0.75$; $K_U = 0.8$
- Three (03) 3-ph motors with power $P = 18.5kW$; $\cos \varphi = 0.90$; $\eta = 0.85$ each. $K_S = 0.75$; $K_U = 0.8$
- A 5kW milling machine of; $\cos \varphi = 0.86$; $\eta = 0.75$; $K_U = 0.8$
- Four (04) 5kW lathes machines, $\cos \varphi = 0.75$; $\eta = 0.85$ each. $K_S = 0.75$; $K_U = 0.8$

Go on to the next page

Workshop C: Carpentry

- A planer of $P = 10kW$; $\cos \phi = 0.85$; $\eta = 0.9$; $K_U = 0.8$
- Nine (09) grinders of: $P = 1.6kW$; $\cos \phi = 0.8$; $\eta = 0.9$ each. $K_S = 0.75$; $K_U = 0.8$
- A jointer of: $P = 7kW$; $\cos \phi = 0.8$; $\eta = 0.9$; $K_U = 0.8 = 7KW$; $\cos \phi = 0.80$; $\eta = 0.9$. $K_U = 0.8$
- Eighteen (18) compensated fluorescent tubes in twin mounting of: $40W$; $\cos \phi = 0.86$ each
- Two (02) sanders of: $P = 1.5kW$; $\cos \phi = 0.80$; $\eta = 0.9$ each. $K_S = 0.75$; $K_U = 0.8$
- Two (02) circular saws of: $P = 3kW$; $\cos \phi = 0.85$; $\eta = 0.75$ each. $K_S = 0.75$; $K_U = 0.8$

Administrative block and Class Room : $K_S = K_U = 1$

- Three (03) air conditioners of: $P = 2.5kW$; $\cos \phi = 0.85$; $\eta = 0.75$ each.
- Twenty-one (21) lighting fittings carrying two fluorescent tubes of: $P = 10kW$; $\cos \phi = 0.86$ each.
- Twelve (12) 1-ph socket-outlets of: $2P + T$; 16A, 220V each.
- Two (02) refrigerators of $P = 2kW$; $\cos \phi = 0.86$; $\eta = 0.75$ each.
- Eight (08) 1-ph socket-outlets of: $2P + T$; 16A, 220V each, in each class room.
- Five (05) lighting fittings carrying two fluorescent tubes of: $P = 40kW$; $\cos \phi = 0.86$ each, in each class room.

NB :

- The power lost in the ballast of each fluorescent tube is estimated at 25% of the rated power of the tube.
- The simultaneity factors to be applied to the whole administrative/classrooms and workshops switchgear console are 1 and 1.
- The ambient temperature of the entire structure is 40 °C.
- For sockets $K_S = 0.1 + \frac{0.9}{N}$ (with $N \leq 5$ number of sockets per circuit) and $K_U = 1$.

Section A. (COMPULSORY)**1. Power demand and choice of transformer**

- a) Complete appendix 1 by calculating the:
 - i. active, reactive, apparent powers absorbed, the currents absorbed and power factors in each block. (5 marks×4)
 - ii. active, reactive, apparent powers absorbed, the total current absorbed in the whole installation and the overall power factor the whole installation (15 marks)
- b) Using appendix 2, choose the appropriate transformer specifying its characteristics, including (S_n , U_{sc} , U_{20} , I_n and I_{sc}) knowing that for reasons of extension of the installation, the power previously calculated as 248 KVA is to be increased by 40%. (5 marks)

Section B**2. Power factor improvement.**

The power factor of the overall installation is to be improved from 0.88 to 0.93. The overall installation active power is assumed to be 220 kW, the rated apparent power (S_n) of the transformer to be 400 kVA.

- a) Determine the corrected power Q_c and the ratio of the correction $\frac{Q_c}{S_n}$ to be installed using appendix 3 and precise the type of compensation. (15 marks)
- b) Use appendix 4 to select:
 - i. the type of network using appendix 4 for $\frac{G_h}{S_n} = 26\%$ (8 marks)
 - ii. the type of compensation for $\frac{Q_c}{S_n} \leq 15\%$. (7 marks)

Turn Over

3. Selection of cables sizes.

Table 1 gives the characteristics of cables. All the cables are made of copper and placed together, under a temperature of 40 °C.

| Cable labelling | Length (m) | Current absorbed (A) (A) | Nature of the insulator | Laying method |
|-----------------|------------|--------------------------|-------------------------|---|
| CS ₀ | 6 | 365 | XLPE | Multi-core cable installed alone on perforated cable tray. |
| CS ₁ | 35 | 320 | XLPE | Multi-core cable placed on perforated tray with 2 other circuits. |
| CS ₂ | 40 | 45 | PVC | Single-core cable laid with 4 other circuits on un-perforated cable tray. |
| CS ₃ | 40 | 130 | XLPE | PVC multicore cable laid alone under spaces in buildings. |

Table 1: Characteristics of cables

| Cable labelling | Insulator | Letter of selection | Correction Factor (k ₁ .k ₂ .k ₃) | Current Absorbed (A) | Current Corrected (A) | C.S.A. (mm ²) |
|-----------------|-----------|---------------------|---|----------------------|-----------------------|---------------------------|
| CS ₀ | | | | | | |
| CS ₁ | | | | | | |
| CS ₂ | | | | | | |
| CS ₃ | | | | | | |

Table 2

Determine, using the manufacturer documents of Appendix 5 and 6, the standard cross sectional area of the cables based on the characteristics provided, by filling in the table 2. (30 marks)

4. Selection of circuit breakers.

- a) Determine, using appendix 7, the length of cables in table 1 and the upstream I_{SC} of the chosen transformer of 14.2kA the downstream short-circuit currents at the following points:
- BB1 busbar; S=185mm² (2.5 marks)
 - BB2 busbar; S=185mm² (2.5 marks)
 - Administrative block and Class Rooms. CS=25mm² (2.5 marks)
- b) Choose the circuit breakers (CB₁, CB₂, CB₃, CB₄ and CB₅) using the manufacturer documents of appendix 8a & 8b by filling table 3. (22.5 marks)

| Labelling | Type (reference) | Calculated current (A) | Nominal Current (A) | Nominal Voltage (V) | Number of poles | Breaking Capacity(kA) |
|-----------------|------------------|------------------------|---------------------|---------------------|-----------------|-----------------------|
| CB ₁ | | 350 | | | | |
| CB ₂ | | 61 | | | | |
| CB ₃ | | 127 | | | | |
| CB ₄ | | 130 | | | | |
| CB ₅ | | 61 | | | | |

Table 3

5. Lighting pre-project

You are also entrusted with the study of the lighting project of the multi-purpose hall which is under construction in the complex, whose characteristics are as follows:

- Size of the multi-purpose hall: 50m × 20m ; working height : 7.20 m ;
- Reflection factor of walls: Ceiling 50%, Wall 30%, Useful plan 30%;
- Average luminance level for general lighting: 300 lux ;
- Light sources: fluorescent mercury vapor lamp or high pressure sodium vapor lamp.

- Lighting fixture: a semi-intensive, bright, anodized aluminum direct reflector capable of using any of the selected sources; $\eta = 0.7$
- Easy maintenance, relatively low total installation cost, low dust level.
- Depreciation factor $d=1,25$.

According to the specifications above, and using appendix 9:

- a. Determine the total luminous flux to be produced. (10 marks)
 - b. Determine the number of devices for each of the proposed sources. (8 marks)
 - c. Choose the most economical solution to determine the number of lamps to install and propose the plan of distribution of the lighting fittings by respecting the standard. (12marks)
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TABLE OF CHARACTERISTICS OF HV/LV TRANSFORMERS.

MAXIMUM SHORT-CIRCUIT CURRENT FROM DOWNSTREAM OF A TRANSFORMER MV/LV

The values indicated in the table below correspond to a three-phase short-circuit bolted at the terminals of a MV/LV transformer connected to a network whose short-circuit power in MV is 500 MVA at 20 kV.

| | Ratings of transformers in KVA | | | | | | | | | | | | | |
|---------------------------|--------------------------------|-----|-----|-----|-----|-----|------|------|------|------|------|------|-------|------|
| | 50 | 63 | 80 | 100 | 125 | 160 | 200 | 250 | 315 | 400 | 500 | 630 | 800 | 1000 |
| 220V | | | | | | | | | | | | | | |
| I_n(A) | 120 | 157 | 200 | 250 | 313 | 400 | 500 | 625 | 789 | 1000 | 1250 | 1575 | 2000 | 2500 |
| I_{sc}(KA) | 3.1 | 3.9 | 4.8 | 6.2 | 7.8 | 9.9 | 12.4 | 15.4 | 19.4 | 24.5 | 31.2 | 38.2 | 38.35 | 44.4 |
| U_{sc}(%) | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | | |
| Copper losses (kW) | 1.1 | 1.1 | 1.1 | 1.8 | 1.8 | 2.4 | 2.85 | 3.25 | 3.9 | 4.81 | 5.95 | 6.95 | 12 | 13.9 |
| 380V | | | | | | | | | | | | | | |
| I_n(A) | 72 | 91 | 115 | 140 | 180 | 232 | 290 | 360 | 450 | 580 | 720 | 910 | 1155 | 1445 |
| I_{sc}(KA) | 1.8 | 2.3 | 2.9 | 3.7 | 4.5 | 5.7 | 7.14 | 8.9 | 11.2 | 14.2 | 17.6 | 22.1 | 24.8 | 27.8 |
| U_{sc}(%) | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4.5 | 5 |
| Copper losses (kW) | 1.1 | 1.1 | 1.1 | 1.8 | 1.8 | 2.4 | 2.85 | 3.25 | 3.9 | 4.81 | 5.5 | 6.95 | 10.2 | 12.1 |

APPENDIX 9 (Q5)

| Ceiling | Reflection Factors (%) | | | | | | | | | | | | | | | |
|-------------|------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|--|
| | 70 | | | 50 | | | 30 | | | 70 | | | 50 | | 0 | |
| | 50 | 30 | 10 | 50 | 30 | 10 | 30 | 10 | 50 | 30 | 10 | 50 | 30 | 0 | | |
| Walls | | | | | | | | | | | | | | | | |
| Useful plan | | | | 10 | | | | | | 30 | | | | | | |
| K | 0.60 | 0.42 | 0.37 | 0.34 | 0.41 | 0.37 | 0.34 | 0.37 | 0.34 | 0.44 | 0.38 | 0.35 | 0.43 | 0.38 | 0.33 | |
| | 0.80 | 0.48 | 0.44 | 0.41 | 0.48 | 0.44 | 0.41 | 0.43 | 0.41 | 0.51 | 0.46 | 0.42 | 0.50 | 0.45 | 0.39 | |
| | 1.00 | 0.54 | 0.50 | 0.47 | 0.53 | 0.49 | 0.46 | 0.49 | 0.46 | 0.57 | 0.52 | 0.48 | 0.56 | 0.51 | 0.45 | |
| | 1.25 | 0.58 | 0.55 | 0.52 | 0.57 | 0.54 | 0.51 | 0.53 | 0.51 | 0.63 | 0.58 | 0.54 | 0.61 | 0.56 | 0.50 | |
| | 1.50 | 0.62 | 0.58 | 0.56 | 0.60 | 0.57 | 0.55 | 0.57 | 0.55 | 0.67 | 0.62 | 0.58 | 0.64 | 0.60 | 0.53 | |
| | 2.00 | 0.66 | 0.64 | 0.61 | 0.65 | 0.63 | 0.61 | 0.62 | 0.60 | 0.73 | 0.66 | 0.65 | 0.70 | 0.66 | 0.59 | |
| 2.50 | 0.69 | 0.65 | 0.69 | 0.68 | 0.66 | 0.64 | 0.65 | 0.63 | 0.77 | 0.73 | 0.70 | 0.73 | 0.70 | 0.62 | | |

Table 4: Utilance Factors

| | Mercury vapour lamp with fluorescent balloon | High pressure sodium lamp |
|----------------------|--|---------------------------|
| Life Span | 6000 hours | 6000 hours |
| Power | 400 W | 400 W |
| Losses due to choke | 22 W | 22 W |
| Flux emitted by lamp | 22.000 Lm | 47.000 Lm |
| Cost of (fixture + | 9000frs CFA | 13500frs CFA |

Table 5: Characteristics of lamps

APPENDIX 3 (Q2a)

REQUIRED REACTIVE POWER KVAR PER KW TO IMPROVE THE POWER FACTOR

The capacitors improve the power factor only on the part of the installation situated before their point of connection. they shall be placed near appliances consuming reactive energy

| Before Improvement | | Power of Capacitor in KVAR to be installed per KW of load to improve the power factor | | | | | | | | | | | | | |
|--------------------|-------------|---|------|------|------|-------|------|-------|------|------|------|------|-------|-------|---|
| $\tan \phi$ | $\cos \phi$ | $\tan \phi$ | 0.75 | 0.59 | 0.48 | 0.46 | 0.43 | 0.4 | 0.36 | 0.33 | 0.29 | 0.25 | 0.20 | 0.14 | 0 |
| $\cos \phi$ | $\cos \phi$ | 0.80 | 0.86 | 0.9 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1 | |
| 2.29 | 0.4 | 1.55 | 1.69 | 1.80 | 1.83 | 1.861 | 1.89 | 1.924 | 1.95 | 1.99 | 2.03 | 2.08 | 2.146 | 2.288 | |
| 2.22 | 0.41 | 1.47 | 1.62 | 1.74 | 1.76 | 1.798 | 1.83 | 1.840 | 1.89 | 1.93 | 1.97 | 2.02 | 2.082 | 2.225 | |
| 2.16 | 0.42 | 1.41 | 1.56 | 1.68 | 1.70 | 1.738 | 1.77 | 1.800 | 1.83 | 1.87 | 1.91 | 1.96 | 2.022 | 2.164 | |
| 2.10 | 0.43 | 1.35 | 1.49 | 1.62 | 1.65 | 1.680 | 1.71 | 1.742 | 1.77 | 1.81 | 1.85 | 1.90 | 1.964 | 2.107 | |
| 2.04 | 0.44 | 1.29 | 1.44 | 1.55 | 1.58 | 1.614 | 1.64 | 1.677 | 1.71 | 1.75 | 1.79 | 1.83 | 1.899 | 2.041 | |
| 1.98 | 0.45 | 1.23 | 1.38 | 1.50 | 1.53 | 1.561 | 1.59 | 1.628 | 1.65 | 1.69 | 1.73 | 1.78 | 1.846 | 1.988 | |
| 1.93 | 0.46 | 1.17 | 1.33 | 1.44 | 1.47 | 1.502 | 1.53 | 1.567 | 1.60 | 1.63 | 1.67 | 1.72 | 1.786 | 1.929 | |
| 1.88 | 0.47 | 1.13 | 1.27 | 1.39 | 1.42 | 1.454 | 1.48 | 1.519 | 1.53 | 1.58 | 1.62 | 1.67 | 1.758 | 1.881 | |
| 1.83 | 0.48 | 1.07 | 1.22 | 1.34 | 1.37 | 1.400 | 1.43 | 1.464 | 1.49 | 1.53 | 1.57 | 1.62 | 1.684 | 1.826 | |
| 1.78 | 0.49 | 1.03 | 1.17 | 1.29 | 1.32 | 1.355 | 1.38 | 1.420 | 1.45 | 1.48 | 1.53 | 1.57 | 1.639 | 1.782 | |
| 1.73 | 0.50 | 0.96 | 1.13 | 1.24 | 1.27 | 1.303 | 1.33 | 1.369 | 1.40 | 1.44 | 1.48 | 1.52 | 1.590 | 1.732 | |
| 1.69 | 0.51 | 0.93 | 1.08 | 1.20 | 1.23 | 1.257 | 1.29 | 1.323 | 1.35 | 1.39 | 1.43 | 1.48 | 1.544 | 1.686 | |
| 1.64 | 0.52 | 0.89 | 1.04 | 1.16 | 1.18 | 1.215 | 1.24 | 1.281 | 1.31 | 1.35 | 1.39 | 1.44 | 1.502 | 1.644 | |
| 1.60 | 0.53 | 0.85 | 1.00 | 1.11 | 1.14 | 1.171 | 1.20 | 1.237 | 1.27 | 1.30 | 1.34 | 1.37 | 1.458 | 1.600 | |
| 1.56 | 0.54 | 0.80 | 0.95 | 1.07 | 1.10 | 1.130 | 1.16 | 1.196 | 1.23 | 1.26 | 1.30 | 1.35 | 1.417 | 1.559 | |
| 1.52 | 0.55 | 0.76 | 0.91 | 1.03 | 1.06 | 1.090 | 1.12 | 1.156 | 1.19 | 1.22 | 1.26 | 1.31 | 1.377 | 1.519 | |
| 1.48 | 0.56 | 0.73 | 0.87 | 0.99 | 1.02 | 1.051 | 1.08 | 1.117 | 1.15 | 1.18 | 1.22 | 1.27 | 1.338 | 1.480 | |
| 1.44 | 0.57 | 0.69 | 0.84 | 0.95 | 0.98 | 1.013 | 1.04 | 1.079 | 1.11 | 1.15 | 1.19 | 1.23 | 1.300 | 1.442 | |
| 1.40 | 0.58 | 0.66 | 0.80 | 0.92 | 0.94 | 0.976 | 1.01 | 1.042 | 1.07 | 1.11 | 1.15 | 1.20 | 1.263 | 1.405 | |
| 1.37 | 0.59 | 0.61 | 0.76 | 0.88 | 0.91 | 0.939 | 0.97 | 1.005 | 1.03 | 1.07 | 1.11 | 1.16 | 1.226 | 1.368 | |
| 1.33 | 0.60 | 0.58 | 0.73 | 0.84 | 0.87 | 0.905 | 0.93 | 0.971 | 1.00 | 1.04 | 1.08 | 1.13 | 1.192 | 1.334 | |
| 1.30 | 0.61 | 0.54 | 0.69 | 0.81 | 0.84 | 0.870 | 0.90 | 0.936 | 0.97 | 1.00 | 1.04 | 1.09 | 1.157 | 1.299 | |
| 1.27 | 0.62 | 0.51 | 0.66 | 0.78 | 0.80 | 0.838 | 0.87 | 0.902 | 0.93 | 0.97 | 1.01 | 1.06 | 1.123 | 1.265 | |
| 1.23 | 0.63 | 0.48 | 0.63 | 0.74 | 0.77 | 0.804 | 0.83 | 0.870 | 0.90 | 0.94 | 0.98 | 1.03 | 1.091 | 1.233 | |
| 1.20 | 0.64 | 0.45 | 0.60 | 0.71 | 0.74 | 0.771 | 0.80 | 0.837 | 0.87 | 0.90 | 0.94 | 0.99 | 1.058 | 1.200 | |
| 1.17 | 0.65 | 0.41 | 0.56 | 0.68 | 0.71 | 0.740 | 0.77 | 0.806 | 0.84 | 0.87 | 0.91 | 0.96 | 1.007 | 1.169 | |
| 1.14 | 0.66 | 0.38 | 0.53 | 0.65 | 0.68 | 0.709 | 0.74 | 0.775 | 0.80 | 0.84 | 0.88 | 0.93 | 0.996 | 1.138 | |
| 1.11 | 0.67 | 0.35 | 0.50 | 0.62 | 0.65 | 0.679 | 0.71 | 0.745 | 0.77 | 0.81 | 0.85 | 0.90 | 0.966 | 1.108 | |
| 1.08 | 0.68 | 0.32 | 0.47 | 0.59 | 0.62 | 0.650 | 0.68 | 0.716 | 0.75 | 0.78 | 0.82 | 0.87 | 0.937 | 1.079 | |
| 1.05 | 0.69 | 0.29 | 0.44 | 0.56 | 0.59 | 0.620 | 0.65 | 0.686 | 0.72 | 0.75 | 0.79 | 0.84 | 0.907 | 1.049 | |
| 1.02 | 0.70 | 0.27 | 0.42 | 0.53 | 0.56 | 0.591 | 0.62 | 0.657 | 0.69 | 0.72 | 0.76 | 0.81 | 0.878 | 1.020 | |
| 0.99 | 0.71 | 0.24 | 0.39 | 0.50 | 0.53 | 0.563 | 0.59 | 0.629 | 0.66 | 0.70 | 0.74 | 0.78 | 0.850 | 0.992 | |
| 0.96 | 0.72 | 0.21 | 0.36 | 0.47 | 0.50 | 0.534 | 0.56 | 0.600 | 0.63 | 0.67 | 0.71 | 0.75 | 0.821 | 0.963 | |
| 0.94 | 0.73 | 0.18 | 0.33 | 0.45 | 0.48 | 0.507 | 0.54 | 0.573 | 0.60 | 0.64 | 0.68 | 0.72 | 0.794 | 0.936 | |
| 0.91 | 0.74 | 0.15 | 0.30 | 0.42 | 0.45 | 0.480 | 0.51 | 0.546 | 0.58 | 0.61 | 0.65 | 0.70 | 0.767 | 0.909 | |
| 0.88 | 0.75 | 0.13 | 0.36 | 0.39 | 0.42 | 0.453 | 0.48 | 0.519 | 0.55 | 0.59 | 0.63 | 0.67 | 0.740 | 0.882 | |
| 0.86 | 0.76 | 0.10 | 0.33 | 0.37 | 0.39 | 0.426 | 0.46 | 0.492 | 0.52 | 0.56 | 0.60 | 0.65 | 0.713 | 0.855 | |
| 0.83 | 0.77 | 0.07 | 0.30 | 0.34 | 0.37 | 0.400 | 0.43 | 0.466 | 0.50 | 0.53 | 0.57 | 0.62 | 0.687 | 0.829 | |
| 0.80 | 0.78 | 0.05 | 0.20 | 0.31 | 0.34 | 0.374 | 0.40 | 0.440 | 0.47 | 0.51 | 0.55 | 0.59 | 0.661 | 0.803 | |
| 0.78 | 0.79 | 0.02 | 0.17 | 0.29 | 0.32 | 0.347 | 0.38 | 0.413 | 0.44 | 0.48 | 0.52 | 0.56 | 0.634 | 0.776 | |
| 0.75 | 0.80 | | 0.15 | 0.26 | 0.29 | 0.321 | 0.35 | 0.387 | 0.42 | 0.45 | 0.49 | 0.54 | 0.608 | 0.750 | |
| 0.72 | 0.81 | | 0.12 | 0.24 | 0.26 | 0.295 | 0.32 | 0.361 | 0.39 | 0.43 | 0.47 | 0.51 | 0.582 | 0.724 | |
| 0.70 | 0.82 | | 0.09 | 0.21 | 0.24 | 0.269 | 0.30 | 0.335 | 0.36 | 0.40 | 0.44 | 0.48 | 0.556 | 0.698 | |
| 0.67 | 0.83 | | 0.07 | 0.18 | 0.21 | 0.243 | 0.27 | 0.309 | 0.34 | 0.38 | 0.42 | 0.46 | 0.530 | 0.672 | |
| 0.65 | 0.84 | | 0.04 | 0.16 | 0.19 | 0.217 | 0.25 | 0.283 | 0.31 | 0.35 | 0.39 | 0.43 | 0.504 | 0.645 | |
| 0.62 | 0.85 | | 0.02 | 0.13 | 0.16 | 0.191 | 0.22 | 0.257 | 0.29 | 0.32 | 0.36 | 0.41 | 0.478 | 0.620 | |
| 0.59 | 0.86 | | | 0.10 | 0.14 | 0.167 | 0.19 | 0.230 | 0.26 | 0.30 | 0.34 | 0.39 | 0.450 | 0.593 | |
| 0.57 | 0.87 | | | 0.08 | 0.11 | 0.141 | 0.17 | 0.204 | 0.23 | 0.27 | 0.31 | 0.36 | 0.424 | 0.567 | |
| 0.54 | 0.88 | | | 0.05 | 0.08 | 0.112 | 0.14 | 0.175 | 0.20 | 0.24 | 0.28 | 0.33 | 0.395 | 0.538 | |
| 0.51 | 0.89 | | | 0.02 | 0.05 | 0.086 | 0.11 | 0.149 | 0.18 | 0.23 | 0.26 | 0.30 | 0.369 | 0.512 | |
| 0.48 | 0.90 | | | | 0.03 | 0.058 | 0.08 | 0.121 | 0.15 | 0.19 | 0.23 | 0.28 | 0.341 | 0.484 | |

Turn Over

Choice of the mode of reactive energy compensation: Global-Partial-Individual.

Three modes of compensations in function of the location of equipment:

- The global compensation is case 1.
- The partial compensation is case 2.
- The individual compensation is case 3.

Choice of the type of compensation: Fixed or Automatic.

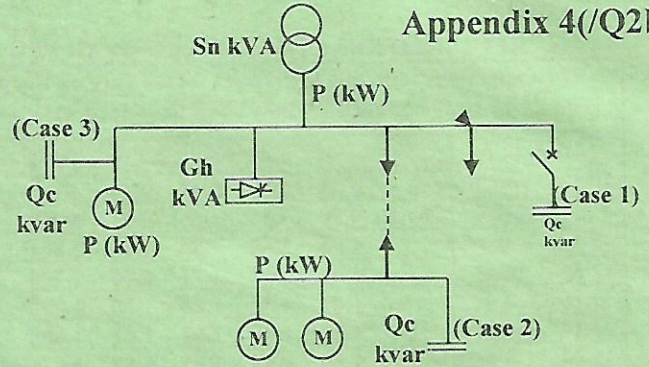
The ratio Q_c/S_n guides in the choice between a fixe compensation equipment or an automatic compensation equipment in the cases of global or partial compensations.

- $Q_c/S_n \leq 15\%$: fixed compensation.
- $Q_c/S_n > 15\%$: automatic compensation.

Selection of the type of reactive energy compensation equipment.

There are three type of compensation equipment based on the level of the harmonic pollution of the network:

- If $G_h/S_n \leq 15\%$, the equipment to use is the **standard** type.
- If $15\% < G_h/S_n \leq 25\%$, the equipment to use is type **H**.
- If $25\% < G_h/S_n \leq 60\%$, the equipment to use is type **SAH**.



S_n : Apparent power of the transformer.

G_h : Apparent power of equipment producing harmonic.

Q_c : Power of the compensation equipment.

| $Q/S \leq 15\%$ Fixe improvement | | Nature of the Network | $Q/S > 15\%$ Automatic improvement | |
|-------------------------------------|---------------------------------|---|---------------------------------------|--|
| Standard type | | Standard network | Standard type | |
| Without protection circuit breaker | With protection circuit breaker | $G_h/S_n \leq 15\%$ | Rectimat | Secomat |
| Varplus M | Rectibloc | | | 22.5 to 180 kVAR Compensation equipment Prisma |
| 10 to 100 kVAR | 10 to 120 kVAR | | 22.5 to 720 kVAR | 150 to 720 kVAR |
| High power Varplus | | $15\% < G_h/S_n \leq 25\%$ | | |
| 100 to 140 kVAR | | | | |
| | | | | |
| Without protection circuit breaker | With protection circuit breaker | $25\% < G_h/S_n \leq 60\%$ | Rectimat | Secomat and Prisma Cabinets |
| Varplus M | Rectibloc | | | 25 to 200 kVAR Compensation equipment Prisma |
| 10 to 100 kVAR | 10 to 120 kVAR | | 22.5 to 720 kVAR | 160 to 540 kVAR |
| High power Varplus | | $12.5 \text{ to } 150 \text{ kVAR}$ $25 \text{ to } 150 \text{ kVAR}$ | | |
| 100 to 140 kVAR | | | | |
| | | | | |

Appendix 5/ Q3

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APPENDIX 5 (Q3)

| REFERENCE METHOD | | |
|-----------------------------|--|------------------|
| Type of cables | Laying Method | Reference method |
| Single or multi-core cables | In visible or embedded conduits and chutes In spaces in buildings, In gutters, mouldings, plinths and frame-linings | B |
| | Directly on the walls or on the ceilings On unperforated cable paths or trays | C |
| Multi-core cables | On corbels, ladder supports and perforated paths Directly on the walls, Suspended cables | E |
| Multi-core cables | On corbels, ladder supports and perforated paths Directly on the walls, Suspended cables | F |

| CORRECTION FACTOR K1 | | |
|----------------------|--|------|
| Reference method | Cases of installation | K1 |
| B | Cables embedded directly in a thermal insulated material | 0.70 |
| | Conduits embedded directly in a thermal insulated material | 0.77 |
| | Multi-core cables | 0.90 |
| | Spaces in buildings and gutters | 0.95 |
| C | Directly fixed on the ceiling | 0.95 |
| B, C, E, F | Other cases | 1 |

| CORRECTION FACTOR K2 | | | | | | | | | | | | | |
|----------------------|---|---|------|------|------|------|------|------|------|------|------|------|------|
| Reference method | Arrangement of joint cables | Correction Factor K2 | | | | | | | | | | | |
| | | Number of circuits or multi-core cables | | | | | | | | | | | |
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 12 | 16 | 20 |
| B,C | Embedded inside the walls | 1.00 | 0.80 | 0.70 | 0.65 | 0.60 | 0.57 | 0.54 | 0.52 | 0.50 | 0.45 | 0.41 | 0.38 |
| C | Single layer on the walls, on the floors or on Unperforated trays | 1.00 | 0.85 | 0.79 | 0.75 | 0.73 | 0.72 | 0.72 | 0.71 | 0.70 | 0.70 | | |
| | Single layer fixed directly under ceiling | 0.95 | 0.81 | 0.72 | 0.68 | 0.66 | 0.64 | 0.63 | 0.62 | 0.61 | 0.61 | | |
| E,F | Single layer on perforated horizontal trays or on vertical trays | 1.00 | 0.88 | 0.82 | 0.77 | 0.75 | 0.73 | 0.73 | 0.72 | 0.72 | 0.72 | | |
| | Single layer on cable ladder supports or cloats | 1.00 | 0.87 | 0.82 | 0.80 | 0.80 | 0.79 | 0.79 | 0.78 | 0.78 | 0.78 | | |

| CORRECTION FACTOR K3 | | | |
|--------------------------|-----------|------|------|
| Ambient Temperature (°C) | Insulator | | |
| | Rubber | PVC | XLPE |
| 10 | 1.29 | 1.22 | 1.15 |
| 15 | 1.22 | 1.17 | 1.12 |
| 20 | 1.15 | 1.12 | 1.08 |
| 25 | 1.07 | 1.07 | 1.04 |
| 30 | 1.00 | 1.00 | 1.00 |
| 35 | 0.93 | 0.93 | 0.96 |
| 40 | 0.82 | 0.87 | 0.91 |
| 45 | 0.71 | 0.79 | 0.87 |
| 50 | 0.58 | 0.71 | 0.82 |

APPENDIX 6 (/Q3)

RECOMMENDED SIMPLIFIED APPROACH FOR CABLE SIZING

| Reference methods | Number of loaded conductors and type of insulation | | | | | | | | | | | | |
|--|--|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | 2 PVC | 3 PVC | | 3 XLPE | 2 XLPE | | | | | | | |
| A1 | | 2 PVC | 3 PVC | | 3 XLPE | 2 XLPE | | | | | | | |
| A2 | 3 PVC | 2 PVC | | 3 XLPE | 2 XLPE | | | | | | | | |
| B1 | | | | 3 PVC | 2 PVC | | 3 XLPE | | 2 XLPE | | | | |
| B2 | | | 3 PVC | 2 PVC | | 3 XLPE | 2 XLPE | | | | | | |
| C | | | | | 3 PVC | | 2 PVC | 3 XLPE | | 2 XLPE | | | |
| E | | | | | | | 3 PVC | | 2 PVC | 3 XLPE | | 2 XLPE | |
| F | | | | | | | | 3 PVC | | 2 PVC | 3 XLPE | | 2 XLPE |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| Size (mm²) Copper | | | | | | | | | | | | | |
| 1.5 | 13 | 13.5 | 14.5 | 15.5 | 17 | 18.5 | 13.5 | 22 | 23 | 24 | 26 | | |
| 2.5 | 17.5 | 18 | 19.5 | 21 | 23 | 25 | 27 | 30 | 31 | 33 | 36 | | |
| 4 | 23 | 24 | 26 | 28 | 31 | 34 | 36 | 40 | 42 | 45 | 49 | | |
| 6 | 29 | 31 | 34 | 36 | 40 | 43 | 46 | 51 | 54 | 58 | 63 | | |
| 10 | 39 | 42 | 46 | 50 | 54 | 60 | 63 | 70 | 75 | 80 | 86 | | |
| 16 | 41 | 43 | 48 | 53 | 58 | 61 | 66 | 73 | 77 | 84 | 91 | | |
| 25 | 68 | 73 | 80 | 89 | 95 | 101 | 110 | 119 | 127 | 135 | 149 | 161 | |
| 35 | | | | 110 | 117 | 126 | 137 | 147 | 158 | 169 | 185 | 200 | |
| 50 | | | | 134 | 141 | 153 | 167 | 179 | 192 | 207 | 225 | 242 | |
| 70 | | | | 171 | 179 | 196 | 213 | 229 | 246 | 268 | 289 | 310 | |
| 95 | | | | 207 | 216 | 238 | 258 | 278 | 298 | 328 | 352 | 377 | |
| 120 | | | | 239 | 249 | 276 | 299 | 322 | 346 | 383 | 410 | 437 | |
| 150 | | | | | 285 | 318 | 344 | 371 | 395 | 441 | 473 | 504 | |
| 185 | | | | | 324 | 362 | 392 | 424 | 450 | 506 | 542 | 575 | |
| 240 | | | | | 380 | 424 | 461 | 500 | 538 | 599 | 641 | 679 | |
| Size (mm²) Aluminium | | | | | | | | | | | | | |
| 2.5 | 13.5 | 14 | 15 | 16.5 | 18.5 | 19.5 | 21 | 23 | 24 | 26 | 28 | | |
| 4 | 17.5 | 18.5 | 20 | 22 | 25 | 26 | 28 | 31 | 32 | 35 | 38 | | |
| 6 | 23 | 24 | 26 | 28 | 32 | 33 | 36 | 39 | 42 | 45 | 49 | | |
| 10 | 31 | 32 | 36 | 39 | 44 | 46 | 49 | 54 | 58 | 62 | 67 | | |
| 16 | 41 | 43 | 48 | 53 | 58 | 61 | 66 | 73 | 77 | 84 | 91 | | |
| 25 | 53 | 57 | 63 | 70 | 73 | 78 | 83 | 90 | 97 | 101 | 108 | 121 | |
| 35 | | | | 86 | 90 | 96 | 103 | 112 | 120 | 126 | 135 | 150 | |
| 50 | | | | 104 | 110 | 117 | 125 | 136 | 146 | 154 | 164 | 184 | |
| 70 | | | | 133 | 140 | 150 | 160 | 174 | 187 | 198 | 211 | 237 | |
| 95 | | | | 161 | 170 | 183 | 195 | 211 | 227 | 241 | 257 | 289 | |
| 120 | | | | 186 | 197 | 212 | 226 | 245 | 263 | 280 | 300 | 337 | |
| 150 | | | | | 226 | 245 | 261 | 283 | 304 | 324 | 346 | 389 | |
| 185 | | | | | 256 | 280 | 298 | 323 | 347 | 371 | 397 | 447 | |

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Appendix 7 (/Q4) DETERMINATION OF SHORT CIRCUIT CURRENT (I_{sc})

The table below shows I_{sc} at a point downstream, as a function of a known upstream fault-current value and the length and c.s.a. of the intervening conductors, in a 220/380V 3-phase system.

| Copper 230 V / 400 V | | | | | | | | | | | | | | | | | | | | | | |
|---|------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|
| c.s.a. of phase conductors (mm ²) | Length of circuit (in metres) | | | | | | | | | | | | | | | | | | | | | |
| 1.5 | | | | | | | | | | | | | | | | | | | | | | |
| 2.5 | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | | | | | | |
| 47.5 | | | | | | | | | | | | | | | | | | | | | | |
| 70 | | | | | | | | | | | | | | | | | | | | | | |
| 95 | | | | | | | | | | | | | | | | | | | | | | |
| 120 | | | | | | | | | | | | | | | | | | | | | | |
| 150 | | | | | | | | | | | | | | | | | | | | | | |
| 185 | | | | | | | | | | | | | | | | | | | | | | |
| 240 | | | | | | | | | | | | | | | | | | | | | | |
| 300 | | | | | | | | | | | | | | | | | | | | | | |
| 2x120 | | | | | | | | | | | | | | | | | | | | | | |
| 2x150 | | | | | | | | | | | | | | | | | | | | | | |
| 2x185 | | | | | | | | | | | | | | | | | | | | | | |
| 55x120 | | | | | | | | | | | | | | | | | | | | | | |
| 3x150 | | | | | | | | | | | | | | | | | | | | | | |
| 3x185 | | | | | | | | | | | | | | | | | | | | | | |
| I _{sc} upstream (in kA) | I _{sc} downstream (in kA) | | | | | | | | | | | | | | | | | | | | | |
| 100 | 93 | 90 | 87 | 82 | 77 | 70 | 62 | 54 | 45 | 37 | 29 | 22 | 17.0 | 12.6 | 9.3 | 6.7 | 4.9 | 3.5 | 2.5 | 1.8 | 1.3 | 0.9 |
| 90 | 84 | 82 | 79 | 75 | 71 | 65 | 58 | 51 | 43 | 35 | 28 | 22 | 16.7 | 12.5 | 9.2 | 6.7 | 4.8 | 3.5 | 2.5 | 1.8 | 1.3 | 0.9 |
| 80 | 75 | 74 | 71 | 68 | 64 | 59 | 54 | 47 | 40 | 34 | 27 | 21 | 16.3 | 12.2 | 9.1 | 6.6 | 4.8 | 3.5 | 2.5 | 1.8 | 1.3 | 0.9 |
| 70 | 66 | 65 | 63 | 61 | 58 | 54 | 49 | 44 | 38 | 32 | 26 | 20 | 15.8 | 12.0 | 8.9 | 6.6 | 4.8 | 3.4 | 2.5 | 1.8 | 1.3 | 0.9 |
| 60 | 57 | 56 | 55 | 53 | 51 | 48 | 44 | 39 | 35 | 29 | 24 | 20 | 15.2 | 11.6 | 8.7 | 6.5 | 4.7 | 3.4 | 2.5 | 1.8 | 1.3 | 0.9 |
| 50 | 48 | 47 | 46 | 45 | 43 | 41 | 38 | 35 | 31 | 27 | 22 | 18.3 | 14.5 | 11.2 | 8.5 | 6.3 | 4.6 | 3.4 | 2.4 | 1.7 | 1.2 | 0.9 |
| 40 | 39 | 38 | 36 | 37 | 36 | 34 | 32 | 30 | 27 | 24 | 20 | 16.8 | 13.5 | 10.6 | 8.1 | 6.1 | 4.5 | 3.3 | 2.4 | 1.7 | 1.2 | 0.9 |
| 35 | 34 | 34 | 33 | 33 | 32 | 30 | 29 | 27 | 24 | 22 | 18.8 | 15.8 | 12.9 | 10.2 | 7.9 | 6.0 | 4.5 | 3.3 | 2.4 | 1.7 | 1.2 | 0.9 |
| 30 | 29 | 29 | 28 | 28 | 27 | 27 | 25 | 24 | 22 | 20 | 17.3 | 14.7 | 12.2 | 9.8 | 7.6 | 5.8 | 4.4 | 3.2 | 2.4 | 1.7 | 1.2 | 0.9 |
| 25 | 25 | 24 | 24 | 24 | 23 | 23 | 22 | 21 | 19.1 | 17.4 | 15.5 | 13.4 | 11.2 | 9.2 | 7.3 | 5.6 | 4.2 | 3.2 | 2.3 | 1.7 | 1.2 | 0.9 |
| 20 | 20 | 20 | 19.4 | 19.2 | 18.8 | 18.4 | 17.8 | 17.0 | 16.1 | 14.9 | 13.4 | 11.8 | 10.1 | 8.4 | 6.8 | 5.3 | 4.1 | 3.1 | 2.3 | 1.7 | 1.2 | 0.9 |
| 15 | 14.8 | 14.8 | 14.7 | 14.5 | 14.3 | 14.1 | 13.7 | 13.3 | 12.7 | 11.9 | 11.0 | 9.9 | 8.7 | 7.4 | 6.1 | 4.9 | 3.8 | 2.9 | 2.2 | 1.6 | 1.2 | 0.9 |
| 10 | 9.9 | 9.9 | 9.8 | 9.8 | 9.7 | 9.6 | 9.4 | 9.2 | 8.9 | 8.5 | 8.0 | 7.4 | 6.7 | 5.9 | 5.1 | 4.2 | 3.4 | 2.7 | 2.0 | 1.5 | 1.1 | 0.8 |
| 7 | 7.0 | 6.9 | 6.9 | 6.9 | 6.8 | 6.7 | 6.6 | 6.4 | 6.2 | 6.0 | 5.6 | 5.2 | 4.7 | 4.2 | 3.6 | 3.0 | 2.4 | 1.9 | 1.4 | 1.1 | 0.8 | 0.8 |
| 5 | 5.0 | 5.0 | 5.0 | 4.9 | 4.9 | 4.9 | 4.8 | 4.7 | 4.6 | 4.5 | 4.3 | 4.0 | 3.7 | 3.4 | 3.0 | 2.5 | 2.1 | 1.7 | 1.3 | 1.0 | 0.8 | 0.8 |
| 4 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.9 | 3.9 | 3.8 | 3.7 | 3.6 | 3.5 | 3.3 | 3.1 | 2.9 | 2.6 | 2.2 | 1.9 | 1.6 | 1.2 | 1.0 | 0.7 | 0.7 |
| 3 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 2.9 | 2.9 | 2.9 | 2.8 | 2.7 | 2.6 | 2.5 | 2.3 | 2.1 | 1.9 | 1.6 | 1.4 | 1.1 | 0.9 | 0.7 | 0.7 | 0.7 |
| 2 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 1.9 | 1.9 | 1.8 | 1.8 | 1.7 | 1.6 | 1.4 | 1.3 | 1.1 | 1.0 | 0.8 | 0.6 | 0.6 | 0.6 |
| 1 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 | 0.8 | 0.8 | 0.7 | 0.6 | 0.6 | 0.5 | 0.5 |
| Aluminium 230 V / 400 V | | | | | | | | | | | | | | | | | | | | | | |
| c.s.a. of phase conductors (mm ²) | Length of circuit (in metres) | | | | | | | | | | | | | | | | | | | | | |
| 2.5 | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | | | | | | |
| 47.5 | | | | | | | | | | | | | | | | | | | | | | |
| 70 | | | | | | | | | | | | | | | | | | | | | | |
| 95 | | | | | | | | | | | | | | | | | | | | | | |
| 120 | | | | | | | | | | | | | | | | | | | | | | |
| 150 | | | | | | | | | | | | | | | | | | | | | | |
| 185 | | | | | | | | | | | | | | | | | | | | | | |
| 240 | | | | | | | | | | | | | | | | | | | | | | |
| 300 | | | | | | | | | | | | | | | | | | | | | | |
| 2x120 | | | | | | | | | | | | | | | | | | | | | | |
| 2x150 | | | | | | | | | | | | | | | | | | | | | | |
| 2x185 | | | | | | | | | | | | | | | | | | | | | | |
| 2x240 | | | | | | | | | | | | | | | | | | | | | | |
| 3x120 | | | | | | | | | | | | | | | | | | | | | | |
| 3x150 | | | | | | | | | | | | | | | | | | | | | | |
| 3x185 | | | | | | | | | | | | | | | | | | | | | | |
| 3x240 | | | | | | | | | | | | | | | | | | | | | | |

Note: for a 3-phase system having 230 V between phases, divide the above lengths by $\sqrt{3}$

Selection of Multi 9 circuit breakers

| Type of circuit breakers | TC16 | TC16P | DPN ⁽⁰⁾ | DPN N | C32H DC | Reflex XC40 | C60a | C60N | C60H | C60L ≤25A | C60L 32-40A | C60L 50-63A | NC100H | NC6100LH |
|---|-------------------|-------------------|--------------------|----------|-----------------------|-------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------|------------|
| Rated current I _n (A) | 16 at 30°C 240 | 16 at 30°C 240 | 240 | 240 | 40 at 30°C Special | 38 at 20°C | 40 at 30°C 440 | 63 at 30°C 440 | 63 at 40°C 440 | 25 at 40°C 440 | 40 at 40°C 440 | 63 at 40°C 440 | 100 at 40°C | 63 at 40°C |
| Rated voltage U _r (V) | 240 | 240 | 60 | 60 | Direct | 250 | 250 | 250 | 250 | 250 | 250 | 250 | 250 | 250 |
| Insulation voltage U _i (V) | 500 | 500 | 500 | 500 | Current | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 |
| Maximum withstand (kV) U _{imp} rated voltage | 6 | 6 | 4 | 4 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| number of poles | 1-1+N | 1-1+N | 1+N | 1+N | 2-3-4 | 2-3-4 | 1 | 2-3-4 | 1 | 2-3-4 | 1 | 2-3-4 | 1 | 2-3-4 |
| Breaking capacity | 3000 | 3000 | 4500 | 6000 | | | | | | | | | | |
| NF C61410 EN 60898 (A eff.) | 230V 400V | 230V/400V | | | | | 3000 | 3000 | 6000 | 10000 | 10000 | | | |
| NF C63120 CEI 947.2 (kA eff.) | 130V | 130V | 6 | 7.5 | | | 10 | 20 | 50 | 50 | 50 | 50 | 100 | 100 |
| | 240V | 4,5 | 4,5 | 2 (400V) | | | 5 | 10 | 10 | 15 | 20 | 20 | 30 | 40 |
| | 415V | | | | | | | | | | | | 154 | 10 |
| | 440V | | | | | | | | | | | | 10 | 40 |
| | | | | | | | | | | | | | 630 | |
| | | | | | | | | | | | | | | |

Selection of NS Compact circuit breakers

| Type of circuit breakers | NS80 | NS125E | NSA160 | NS100 | NS160 | NS250 | NS400 |
|--|------|--------|--------|-------|-------|-------|-------|
| number of poles | 3 | 3,4 | 3,4 | 2,3,4 | 2,3,4 | 2,3,4 | 3,4 |
| Electrical characteristics according to CEI 947-2 and EN 60947-2 | | | | | | | |
| Rated current I _n (A) at 40°C | 80 | 125 | 160 | 100 | 160 | 250 | 400 |
| Insulation voltage U _i (V) | 750 | 750 | 500 | 750 | 750 | 750 | 750 |
| Maximum withstand (kV) U _{imp} rated voltage | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Rated voltage U _r (V) | 690 | 500 | 500 | 690 | 690 | 690 | 690 |
| ac 50/60 Hz | | | | | | | |
| dc | | | | | | | |
| Ultimate breaking capacity I _{cu} (kA _{eff}) | H | E | N | N | N | N | L |
| ac 50/60Hz/220V/240V/10 | 10 | 25 | 50 | 85 | 100 | 150 | 150 |
| 380V/415V/70 | 16 | 30 | 30 | 25 | 70 | 150 | 150 |
| 440V | 65 | 10 | 15 | 25 | 65 | 130 | 130 |
| 500V | 25 | 6 | 18 | 18 | 50 | 70 | 70 |
| 525V | 25 | | 18 | 18 | 35 | 50 | 50 |
| 660/690V | 6 | | 8 | 8 | 10 | 20 | 20 |
| 250V | | | 50 | 50 | 85 | 100 | 100 |
| 500V | | | 50 | 50 | 85 | 100 | 100 |

APPENDIX 8b (Q4b)

Turn Over